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Appropriate Number of Center Points for Response Surface Exploration Using Small Box Behnken Design

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Authors' contributions

This work was carried out in collaboration among all authors. All authors read and approved the final manuscript.

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ABSTRACT

Industrial exploration using the Box Behnken Design (BBD) has been faced with a serious setback due to the swift upsurge in the runs size as the number of factors increase. This, therefore, dissuades researchers and affects the application of the design. The Small Box Behnken Designs (SBBD) which achieve the research goal of BBD were proposed to overcome the setback. This paper aimed at recommending an appropriate number of center points suitable for response surface exploration and its applications in industries using the SBBD. The method adopted for assessing the center points is the prediction variance-based G-efficiency optimality criterion. The range of design factors, k, considered is 3 to 11, while comparing the designs at 0 - 5 number of center points. For each of the design factors considered, the result showed that increasing the

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center point, decreases the G-efficiency value. Hence, increasing the center point does not contribute significantly to the prediction variance capability of the designs considered. However, in other to test the model lack of fit and estimate pure error which are very important in experimental design analysis, this study recommends that at most two runs (center points) be replicated at the center. Since with this number, approximately 90% G-efficiency can be achieved for response surface exploration using the SBBD.

Keywords: Small box behnken design; center point; prediction variance; G-efficiency; optimality.

1. INTRODUCTION

Zhang et al. [1], developed the SBBD as an alternative to the BBD with the aim of achieving similar and effective result as BBD. The SBBD possesses reasonably high D-efficiency, much smaller runs size compared to BBD, and preserved the original orthogonality property of the BBD. Hence, the designs are preferred to BBD for fitting the second-order response surface model [2] investigated the percentage rotatability for evaluating the SBBD using the measure of rotatability introduced by Khuri (1988). They observed that factors k, the SBBD is rotatable for k = 3 factors, near rotatable for k = 4, 7 factors and not rotatable for k = 5, 6, 8, 9, 10 and 11 factors. However, no work has been done on recommending the number of center points suitable for evaluating the SBBD and this form the basics for this work.

Considering that all variables in the response surface model measurable, the expressions in (1) and (2) for first-order response surface model and second-order response surface model respectively are used to quantify the relationship between the controllable input parameters (x_i) and the obtained response surfaces (T) in Response Surface Methodology.

$$T = \tau_0 + \sum_{i=1}^{k} \tau_i x_i + \xi$$
 (1)

$$T = \tau_0 + \sum_{i=1}^{k} \tau_i x_i + \sum_{i < j} \tau_{ij} x_i x_j + \sum_{i=1}^{k} \tau_{ii} x_i^2 + \xi \quad (2)$$

where, *T*, is an $N \times 1$, vector of responses, *x*, is an $N \times P$, of the design matrix. The τ and ξ consist of coefficients of the design factors under consideration and errors term, with dimension $P \times 1$ and $N \times 1$ respectively.

2. OPTIMALITY CRITERIA

It is important to note the fact that a design performs better than other designs under certain

optimality criterion does not always guarantee that it will retain such performance when considered by other optimality criteria. Hence, to choose a design, attention will be on the choice of design evaluation criteria used. The common optimality criteria used in design evaluation are A-, D-, E- and G- optimality criteria, [4,5] in a comparative study of five varieties of CCDs -Central Composite designs (SCCD, RCCD, OCCD, Slope-R, FCC) in RSM, evaluated the performances of the designs using the D-, A-, Gand IV-optimality criteria. The results showed a reduction in the D- and G-optimality criteria, an increase in the A-optimality criterion while the IVoptimality remain relatively the same of the CCDs in all the factors that were considered at different number of center points. [6], evaluate and compare the performances of three classes of Central Composite Design CCDs (CCCD, CCFD and CCID) using the A-, D-, and Gefficiencies for factors, k, that ranges from 3 to 10, with 0-5 center points. It was shown from the results that, for the three CCDs compared, the Gefficiency outperformed other efficiency criteria employed for all the factors and center points considered. [7], applied the D- and G-optimal criteria on non-pure blends slope designs to study the second-order Kronecker model on Equally Weighted Simplex Centroid Axial Design and Un-equally Weighted Simplex Centroid Axial Design. It was shown from the result that the Dand G-optimality values performed better on both centroid compared.

3. CENTER POINTS

The center points are observations collected at the center of all factor ranges, $x_i = 0$, (i = 1, 2, ..., k). These replicated points at the center of all factors are among other things, used to calculate the pure error of second-order models, to check for curvature and to provide a measure of process stability and inherent variability: see [8]. According to [9], center points adds to the estimation of the coefficients of quadratic terms and are used to identify curvature in the response. [10], opined that in other to avoid singularity in the information matrix of a design, effort should be to add center runs to the design so as to maintain favorable design qualities such as good prediction variance. [11], tested the effect of varying the number of center points on parameters estimation by employing the optimality criteria A-, D-, and E. [12] used integrated variance criterion to determine appropriate number of center points for response surface designs; he concluded that fewer center points are appropriate. [13] recommended different number of center point, ranging from 3 to 12 for the Box Behnken Designs. [14], examined the contributions of center points on prediction variance performances on CCDs using the G-optimal, I optimal and FDS plots. It was discovered that the designs perform better with or without replication (center points).

4. EVALUATION OF THE APPROPRIATE NUMBER OF CENTER POINTS

In this section, center points ranging from 0 to 5 will be compared for design factors, k, ranging from 3 to 11, using the G-efficiency criteria. Let, n_o , indicate the number of center points and N, the number of design runs.

The expanded design matrix for SDDB for k = 3, with $n_o = 0$ is;

	[1	-1	-1	0	1	0	0	1	1	0			
<i>X</i> =	1	1	-1	0	-1	0	0	1	1	0			
	1	-1	1	0	-1	0	0	1	1	0			
	1	1	1	0	1	0	0	1	1	0			
	1	-1	0	-1	0	1	0	1	0	1			
	1	1	0	-1	0	-1	0	1	0	1			
	1	-1	0	1	0	-1	0	1	0	1			
	1	1	0	1	0	1	0	1	0	1			
	1	0	-1	-1	0	0	1	0	1	1			
	1	0	1	-1	0	0	-1	0	1	1			
	1	0	_1	1	0	0	_1	0	1	1			
	1	0	1	1	0	0	1	0	1	1			
	L	U		1	0	0	1	U	1		C 42271E + 14	C 42271E + 14	C 42271E + 14]
		1.286/4E+15		0 125	0	0	0		0	0	- 0.433/1E + 14	- 0.433/1E + 14	- 0.433/1E + 14
		0		0.125	0	0	0		0	0	0	0	0
		0		0	0.125	0	0		0	0	0	0	0
		0		0	0	0.12	5 0	_	0	0	0	0	0
(X'X)	-1 =	0		0	0	0	0.12	5	0	0	0	0	0
· /		0		0	0	0	0		0.125	0	0	0	0
		0		0	0	0	0		0	0.125	0	0	0
		- 6.43371E +14		0	0	0	0		0	0	3.21686E+14	3.21686E+14	3.21686E+14
		- 6.43371E + 14		0	0	0	0		0	0	3.21686E + 14	3.21686E+14	3.21686E+14
		- 6.43371E + 14		0	0	0	0		0	0	3.21686E+14	3.21686E+14	3.21686E+14



The G-efficiency is obtained by $100 \frac{p'_N}{\sigma^2_{\max}}$, where, σ^2_{\max} is the maximum prediction variance, N is the number of design runs and P is the number parameters for each of the design considered.

The same procedure was used to obtain the Gefficiencies for all the factors at different center points. The results for the G-efficiency for 0 - 5 center points for each of the factors under consideration are shown in Table 1.

From Table 1, it could be seen that additional center points to each of the designs under consideration rather decreases the G-efficiency, hence, there is no need increasing the number of center points. However, for error estimation which is very important in experimental analysis, one or two center points are recommended since with this number, one can still achieve approximately 90% G-efficiency.









Table 1. Result of G-eff	iciency values	for 0 – 5	center	point

K	Р	Ν	Max[x'(X'X)x]	n_{+0}	<i>n</i> ₊₁	n_{+2}	<i>n</i> ₊₃	n_{+4}	<i>n</i> ₊₅
3	10	12	0.7500	111.11	102.56	95.24	88.89	83.33	78.43
4	15	16	1	93.75	88.24	83.33	78.94	75.00	71.43
5	21	24	0.8889	98.44	94.50	90.86	87.50	84.37	81.46
6	28	32	0.9167	95.45	92.56	89.84	87.27	84.85	82.55
7	36	40	1	90.00	87.81	85.71	83.72	81.82	80.00
8	45	56	0.9670	83.10	81.64	80.23	78.87	77.56	76.29
9	55	60	0.9333	98.22	96.61	95.05	93.54	92.08	90.66
10	66	76	0.9153	94.88	93.65	92.45	91.28	90.13	89.02
11	78	96	0.8967	90.61	89.68	88.76	87.86	86.99	86.12

The graphical assessment of the G-efficiency at 0 to 5 center point, show a decrease in the G-efficiency value as the center point rises and this result was consistent for all the factors under consideration.

5. CONCLUSION

This study has examined the appropriate number of center points required for response surface exploration using the SBBD. It can be concluded from the result that as the number of center point rises from 0 - 5, the G-efficiency decreases. This finding is in agreement with the findings of [6], where the G-efficiency performed better than other alphabet based optimality criteria and in particular, the G-efficiency decreases as number of center pointer increases for CCFD. The implication of this finding suggests that increasing the center point does not contribute significantly to the prediction variance capability of the designs considered. However, for the estimation of pure error and test of model lack of fit, this study recommends that at most two runs (center points) be replicated for response surface exploration using the Small Box Behnken Designs.

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COMPETING INTERESTS

Authors have declared that no competing interests exist.

REFERENCES

- 1. Zhang TF, Yang JF, Lin DKI. Small Box Behnken Design. Statistics and Probability Letter. 2011;81:1027-1033.
- Lawrence CK, Bartholomew DC, Kiwu-Lawrence FC, Obite CP, Okafor IB. Evaluating Percentage Rotatability for The Small Box – Behnken Design. Journal of Mathematics and Statistics Studies. 2021;16 – 24. ISSN: 2709-4200 DOI:10.32996/jmss
- Montgomery DC. Design and Analysis of Experiments.6th ed. John Wiley and Sons Inc, N.J.; 2005.
- 4. Atkinson AC, Donev AN. Optimum Experimental Designs. Oxford University Press, New York; 1992.

- 5. Oyejola BA, Nwanya JC. Selecting the Right Central Composite Design. International Journal of Statistics and Applications. 2015;5(1):21-30. DOI:10.5923/j.statistics.20150501.04
- Kiwu-Lawrence FC, Kiwu LC, Bartholomew DC, Obite CP, Akanno FC. Evaluation and Comparison of Three Classes of Central Composite Designs. Asian Journal of Probability and Statistics. 2021;13(2):31-47.

DOI: 10.9734/AJPAS/2021/v13i230304.

- Njoroge EW, Koske J, Mutiso J. D- and G-Optimal Axial Slope Designs for Four Ingredient Mixture. Applied Mathematics and Physics. 2020;8(1):20-25. DOI: 10.12691/amp-8-1-4
- 8. NIST/SEMATECHHandbook of Statistical Methods; 2003. Available:http://www.itl.nist.gov/div898/han dbook
- Marcin D, Mario D, Terese L. Application of a Central Composite Design for the Study of NOx Emission Performance of a Low NOx Burner. Energies. 2015;8:3606-3627. DOI:10.3390/en8053606
- Myers RH, Montgomery DC, Anderson-Cook CM. Response Surface. Methodology: Process and Product Optimization using designed experiments. 3rd Edition. John Wiley & Sons, Inc. New Jersey; 2009.
- Kasina MM, Joseph K, John M. Application of Central Composite Design to Optimize Spawns Propagation. Open Journal of Optimization. 2020;9:47-70. Available:https://doi.org/10.4236/ojop.2020 .93005.
- 12. Draper NR. Center Points in Second-Order Responds Surface Designs. Technometrics. 1982;24 (2):127 - 133.
- Box GEP, Behnken DW. Some New Three Level Designs for the Study of Quantitative Variables. Technometrics. 1960;2(4):455 -475.
- Nwanya JC, Dozie KCN. Optimal Prediction Variance Capabilities of Inscribed Central Composite Designs. European Journal of Statistics and Probability. 2020;8(2):41-48.

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